

# Design and Construction of a Solar Thermal Absorber Pot Suitable for Use in Parabolic Solar Cookers

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## Abstract

*The mathematical approach to the design and construction of a solar thermal absorber pot and a parabolic dish solar cooker were discussed in this paper. One (1 kg) of rice was used as a measured value for calculating the volume of rice that was used to calculate the volume of pot which aided in determining the dimensions of the pot. Aluminium of thickness 0.55 mm was used for the construction because of its known thermal conductivity and specific heat capacity. Based on these, the effective area of the pot and aperture area of parabolic dish were obtained as 0.1199 m<sup>2</sup> and 0.9505 m<sup>2</sup> respectively. The geometric concentration ratio for the dish solar cooker is calculated as 7.929. The time needed to cook 1 kg of rice with this pot under this cookers at solar radiation intensity of 700 W/m<sup>2</sup> is 1.30 hour.*

**Key words:** Dimension, aperture area, effective area, geometric concentration ratio, thermal conductivity and radiation.

## 1. Introduction

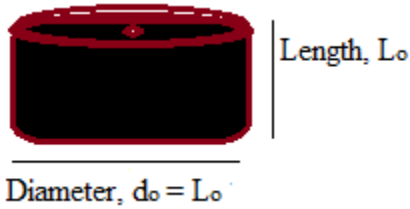
The thermal modelling of solar cookers are characterized by heat and mass transfer, effects of wind, relative humidity, relative movement of the sun, nature of food, types and size of pot fit for the cooking, characteristic of different designs and heat transfer to the surroundings. Cloudy conditions, marginal insolation, tilting position of cooker or mirror's array to capture incoming radiation and wind combined to make concentrating cookers highly difficult to use (Kundapur, 1998; Mmuthusiyagani, 2010; Yahuzat al2016; Tiwari, 2014 and Pidwimy, 2006). But when the pot size and its position fitted to the geometric design of the solar cookers, then challenge of effectiveness and difficulties of using solar cookers becomes minimal except for the weather conditions which are natural phenomena that is beyond human control.

The dimension of cookers and its components such as absorber pots, aperture and depth of the cookers, position of the principal focus above the through of the dish, etc; matter a lot in determining the effective use and delivery of heat to the intended goal of the designed solar cooker (Agyenum, 2009 and Joshua, 2013).

## 2. Methodology

The desired materials needed to achieve the designs and construction of the pot and the solar cooker are: sheet of Aluminium of thickness 0.55 mm (to be used for the construction of both the bodies of the parabolic dish), mirrors and metallic stand for the dish. All these materials are to be used based on the recommended dimensions given in the design procedures of each of them.

### 2.1 Design of the absorber pot



**Figure 1: Schematic diagram of the pot**

For a cylindrical pot shape with the following dimensions:  $d_o$  as the external diameter,  $L_o$  effective length/height (assumed to be equal to  $d_o$ ),  $d_i$  internal diameter,  $L_i$  internal length (assumed to be equal to  $d_i$ ) and  $w$  the thickness of the pot, then the volume  $V_{pot}$  of the pot which is also assumed to be equal to the volume of the food to be cooked is given as:

$$V_{pot} = \frac{\pi d_i^2 L_i}{4} \tag{1}$$

### 2.2 Thermal performance of solar cooker.

The heat demand loads of the cooker is such that it can cook a given mass of rice  $M_{rice}$  at once at a given time. For these designs (pot and parabolic dish), 1 kg of rice is used, same method can be applied to any food once their densities and optimum expansions in terms of food-to-water ratio by volume are given. The only variation to be experienced may be the cooking time duration, one may take longer time than the other based on their nature. If the density of rice to be cooked is  $\rho_{rice}$ , the volume of rice,  $V_{rice}$  is given as:

$$V_{rice} = \frac{M_{rice}}{\rho_{rice}} \tag{2}$$

According to Bhattachary (1972), cited in Okoro (2015), density of rice varies between  $777 - 847 \text{ kgm}^{-3}$  due to the different varieties of rice. Using an average value of  $812 \text{ kgm}^{-3}$  and noting that  $M_{rice}$  is 1 kg, then

$$V_{rice} = \frac{M_{rice}}{\rho_{rice}} = \frac{1}{812} = 1.2315 \times 10^{-3} \text{ m}^3 \tag{3}$$

According to Green (2013) and Nguyenn (2009), volume of cooked rice including water expand by 3.2 – 3.5 times the volume of uncooked dry rice.

By taken 3.35 as an average expansion ratio, the volume of pot required to accommodate the cooked rice will be:

$$V_{cff} = 3.35 V_{rice} = 4.1256 \times 10^{-3} \text{ m}^3 \tag{4}$$

Thus volume of pot is  $V_{pot} = V_{eff}$  and the internal diameter of the pot can be determined from equation (5):

$$V_{pot} = \frac{\pi d_i^2 L_i}{4} = 4.1256 \times 10^{-3} \text{ m}^3 \tag{5}$$

This implies that the internal diameter of the pot  $d_i = 0.17382$  m, the external diameter  $d_o$  and the pot's height  $L_o$  can be determined as:

$$d_o = d + 2w = 0.17382 + 2 \times 0.00055 = 0.1749 \text{ mand}$$

$$L_o = L_i + w = 0.17382 + 0.00055 = 0.1744 \text{ m} \tag{6}$$

where  $w$  is the thickness (0.55 mm) of the pot.

Therefore, effective area  $A_{eff}$ :

$$A_{eff} = \frac{\pi d_o^2}{4} + \pi d_o L_o = \frac{3.142(0.17492)^2}{4} + 3.142 \times 0.17492 \times 0.17437 = 0.1199 \text{ m}^2 \tag{7}$$

Area of the rim  $A_{p-rim}$  of the pot and its lid cover  $A_{lcov}$  are obtained as:

$$A_{p-rim} = \pi r_o^2 - \pi r_i^2 = 3.0133 \times 10^{-4} \text{ m}^2 \tag{8}$$

$$A_{lcov} = \pi r_o^2 = 0.02403 \text{ m}^2 \tag{9}$$

According to Dilipet *al* (2014), the optimum rice-to-water ratio by volume is given as 2:3.2. Thus the volume of water  $V_w$  required to cook the given volume of rice  $V_{rice}$  is:

$$V_w = \frac{3.2}{2} V_{rice} = 1.6 \times 1.23153 \times 10^{-3} = 1.9705 \times 10^{-3} \text{ m}^3 \tag{10}$$

Total volume of uncooked food  $V_{uf}$  is given as:

$$V_{uf} = V_w + V_{rice} = 2.6 V_{rice} = 2.6 \times 1.23153 \times 10^{-3} = 3.2020 \times 10^{-3} \text{ m}^3 \tag{11}$$

Mass of water required  $M_w$  (From appendix A,  $\rho_w = 995.8 \text{ kg/m}^3$  at  $27^\circ\text{C}$ ) is:

$$M_w = \rho_w V_w = \rho_w \frac{3.2}{2} V_{rice} = 995.8 \times 1.6 \times 1.23153 \times 10^{-3} = 1.9622 \text{ kg} \tag{12}$$

Therefore the total mass of uncooked food is given by:

$$M_{uf} = M_w + M_{rice} = 1.96217 + 1 = 2.9622 \text{ kg} \tag{13}$$

Ratio of cooked food to uncooked food is

$$\frac{V_{eff}}{V_{uf}} = \frac{3.35 V_{rice}}{2.6 V_{rice}} = 1.2885$$

$$V_{eff} = 1.2885 V_{uf} \tag{14}$$

This means that after cooking, the volume of food increased by 29 %.

In conventional methods of cooking, about 25 % of water required for cooking is lost to the surrounding through evaporation (Mahavar, 2013).

If the amount of water lost is taken as a direct proportion to the amount of water required, then the amount of water lost during cooking with solar cooker is 25 %. Thus, mass of water remaining  $M_{w,rem}$  and mass of water lost  $M_{lost}$  during cooking with solar are equal to:

$$M_{w,rem} = (1 - 0.25)M_w = 0.75 \times 1.96217 = 1.4716 \text{ kg} \tag{15}$$

Mass of water lost:

$$M_{lost} = 1.96217 - 1.4716 = 0.4906 \text{ kg} \quad (16)$$

Therefore, total mass of cooked food,  $M_{TCF}$  is:

$$M_{TCF} = M_{rice} + M_{w,rem} = 1 + 1.4716 = 2.4716 \text{ kg} \quad (17)$$

Ratio of cooked food to uncooked food is:

$$\frac{M_{TCF}}{M_{uf}} = \frac{2.4716}{2.96217} = 0.8344 \quad (18)$$

Mass of initial uncooked food decreased by:  $(1 - 0.83439) \times 100\% = 16.56\%$

Estimated rate of energy to be absorbed by the food under the solar cooker is:

$$Q_{ab} = \eta_{th} I_b A_{ap} \quad (19)$$

where  $A_{ap}$  is the aperture area and  $I_b$  the average solar intensity at the location. Assuming thermal efficiency of solar cookers to be 50 – 70 %, therefore average thermal efficiency will be 60 %,  $I_b$  is 700 W/m<sup>2</sup> (ASAE, 2013 & Funk, 2000). In this work a parabolic dish of depth  $h = 25$  cm and aperture diameter  $D = 1.1$  m (110 cm) is used.

Hence, aperture area  $A_{ap}$  is given as:

$$A_{ap} = \frac{\pi D^2}{4} = 0.9505 \text{ m}^2$$

$$Q_{ab} = 0.6 \times 700 \times 0.9505 = 399.1911 \text{ W} \quad (20)$$

Rate of energy absorbed by pot is given as:

$$Power = \eta_o I_b A_{ap} = \frac{\eta_o}{\eta_{th}} (\eta_{th} A_{ap} I_b) = \frac{\eta_o}{\eta_{th}} \cdot Q_{ab} \quad (21)$$

Taking optical efficiency to be 0.6 as the lower fraction of 0.6 and 0.7, thus

$$power = \frac{0.7}{0.6} \times 399.1911 = 465.7230 \text{ W} \quad (22)$$

In this design, the latent heat of vaporization of water is considered as part of the useful energy. The useful energy,  $Q_u$  required for the cooking is given as:

$$Q_u = Q_1 + Q_2 \quad (23)$$

where  $Q_1$  is the heat required to rise the sensible temperature of food to 100 °C, and  $Q_2$  is the heat energy required to convert (0.4905 kg) the loss mass of water at 100 °C to steam and given as:

$$Q_1 = (M_w + M_{rice}) \cdot C_w (T_{w2} - T_{w1}) = \eta_{th} I_b A_{ap} \cdot t_1 \quad (24)$$

where  $t_1$  is the time required to raise the temperature of the food from  $T_{w1}$  (assumed 27°C) to  $T_{w2}$  (100 °C). Thus

$$t_1 = \frac{M_{TCF} C_w (T_{w2} - T_{w1})}{\eta_{th} I_b A_{ap}} = \frac{2.4716 \times 4186 \times (100 - 27)}{0.6 \times 700 \times 0.9505} = 1,891.9030 \text{ s} = 0.5255 \text{ hr} \quad (25)$$

$$Q_2 = M_w \cdot L_w = \eta_{th} \cdot I_B \cdot A_{ap} \cdot t_2 \tag{26}$$

where  $L_w$  is the latent heat of vaporization of water at 100 °C and  $t_2$  is the time required to convert 0.4905 kg mass of water to steam (Agyenum, 2009). Thus

$$t_2 = \frac{M_w L_w}{\eta_{th} I_B A_{ap}} = \frac{0.4905 \times 2.26 \times 10^6}{0.6 \times 700 \times 0.9505} = 2,776.8092 \text{ s} = 0.7713 \text{ hr} \tag{27}$$

Total time  $t$  required for cooking is therefore given as:

$$t = t_1 + t_2 = 0.5255 + 0.7713 = 1.2968 \text{ hr} \tag{28}$$

### 2.3 Design of Parabolic Dish

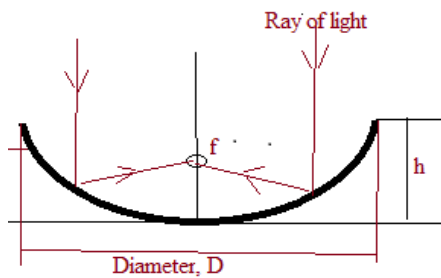


Figure 2: Sketch of parabolic dish

The dimension of symmetrical parabolic solar cooker can be estimated (Aidan 2014 and Okoro 2015) as:

$$h = \frac{R_{rim}^2}{4f} \tag{29}$$

where  $h$  is the depth of the parabolic dish,  $R_{rim}$  is the rim radius ( $R_{rim} = \frac{D}{2}$ ),  $D$  is the aperture diameter of the parabolic cooker and  $f$  is the focal length.

$$f = \frac{R_{rim}^2}{4h} = \frac{(55)^2}{4 \times 25} = 30.25 \text{ cm} \tag{30}$$

The rim angle  $\theta_{rim}$  can be estimated as:

$$\theta_{rim} = \tan^{-1} \left( \frac{1}{\frac{D}{8h} - \frac{2h}{D}} \right) = \tan^{-1} \left( \frac{1}{\frac{110}{8 \times 25} - \frac{2 \times 25}{110}} \right) = \tan^{-1}(10.476190) = 84.55^\circ \tag{31}$$

The geometric concentration ratio of the dish with respect to the effective area of the pot is given as:

$$C_{dish-g} = \frac{A_{ap}}{A_{eff}} = \frac{\pi D^2}{4A_{eff}} = \frac{3.142(1.1)^2}{4 \times 0.11987} = 7.93 \tag{32}$$

The surface area of the parabolic dish can be determined (Quedermi et al 2009) from:

$$A_s = \frac{4\pi f^2 \sin^2 \theta_{rim}}{1 + \cos \theta_{rim}} \cong \frac{8\pi}{3} f^2 \left[ \left( \left( 1 + \left( \frac{D}{4f} \right)^2 \right)^{3/2} - 1 \right) \right]$$

$$= \frac{8 \times 3.142(30.25)^2}{3} \left[ \left( \left( 1 + \left( \frac{110}{4 \times 30.25} \right)^2 \right)^{3/2} - 1 \right) \right] = 11,258.00233 \text{ cm}^2 = 1.1258 \text{ m}^2(33)$$

### 3. Conclusion

From the above analysis, the geometric concentration ratio for the parabolic solar cooker to the effective area of the pot ( $A_{eff} = 0.1199 \text{ m}^2$ ) is calculated to be 7.929. The time needed to cook 1 kg of rice with this pot when used in this cookers based on its thermal performance at solar radiation of  $700 \text{ W/m}^2$  is 1.30 hour. This shows that the cooker and the pot of such dimensions can achieve cooking within the short possible period of time when all controlled and uncontrolled variables are not interrupted during their usage in cooking.

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**Appendix A**

**Table 1: Properties of water (saturated liquid)**

°F	°C	$c_p$ kJ/kg°C	$\rho$ Kg/m <sup>3</sup>	$\mu$ kg/m sec	$K$ W/m°C	Pr	$V = \mu/\rho$ m <sup>2</sup> /s
32	0	4.225	999.8	1.79x10 <sup>-3</sup>	0.566	13.25	1.79x10 <sup>-6</sup>
40	4.44	4.208	999.8	1.55x10 <sup>-3</sup>	0.575	11.35	1.55x10 <sup>-6</sup>
50	10	4.195	999.2	1.31x10 <sup>-3</sup>	0.585	9.40	1.31x10 <sup>-6</sup>
60	15.56	4.186	998.6	1.12x10 <sup>-3</sup>	0.595	7.88	1.12x10 <sup>-6</sup>
70	21.11	4.179	997.4	9.8 x 10 <sup>-4</sup>	0.604	6.78	9.82x10 <sup>-7</sup>
80	26.67	4.179	995.8	8.6 x 10 <sup>-4</sup>	0.614	5.85	8.63x10 <sup>-7</sup>
90	32.22	4.174	994.9	7.65x10 <sup>-4</sup>	0.623	5.12	7.69x10 <sup>-7</sup>
100	37.78	4.174	993.0	6.82x10 <sup>-4</sup>	0.630	4.53	6.87x10 <sup>-7</sup>
110	43.33	4.174	990.6	6.16x10 <sup>-4</sup>	0.637	4.04	6.22x10 <sup>-7</sup>
120	48.89	4.174	988.8	5.62x10 <sup>-4</sup>	0.644	3.64	5.68x10 <sup>-7</sup>
130	54.44	4.179	985.7	5.13x10 <sup>-4</sup>	0.649	3.30	5.20x10 <sup>-7</sup>
140	60	4.179	983.3	4.71x10 <sup>-4</sup>	0.654	3.01	4.63x10 <sup>-7</sup>
150	65.55	4.183	980.3	4.3 x 10 <sup>-4</sup>	0.659	2.73	4.39x10 <sup>-7</sup>
160	71.11	4.186	977.3	4.01x10 <sup>-4</sup>	0.665	2.53	4.10x10 <sup>-7</sup>
170	76.67	4.191	973.7	3.72x10 <sup>-4</sup>	0.668	2.33	3.82x10 <sup>-7</sup>
180	82.22	4.195	970.2	3.47x10 <sup>-4</sup>	0.673	2.16	3.58x10 <sup>-7</sup>
190	87.78	4.199	966.7	3.27x10 <sup>-4</sup>	0.675	2.03	3.38x10 <sup>-7</sup>
200	93.33	4.204	963.2	3.06x10 <sup>-4</sup>	0.678	1.90	3.18x10 <sup>-7</sup>
210	104.4	4.216	955.1	2.67x10 <sup>-4</sup>	0.684	1.66	2.79x10 <sup>-7</sup>

Courtesy: G.N. Tiwari (2014). Centre for Energy Studies, New Delhi 110016, India