

Analysis and Control of DC Microgrid Using Quadratic Boost Converter with Intelligent Controllers

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Abstract:

This paper presents the modeling, simulation, and comparative analysis of a DC microgrid system under healthy and faulty conditions. The system incorporates renewable energy sources such as PV, wind, fuel cells, and battery storage, regulated through a Quadratic Boost Converter (QBC). Faults including shorted switch, line-to-line, and line-to-ground conditions are analyzed through MATLAB/Simulink simulations. Control strategies including Proportional-Integral (PI), Fractional Order PID (FOPID), and Fuzzy Logic (FL) controllers are implemented to regulate output parameters. The FOPID and FL controllers showed improved transient response compared to conventional PI control. Results demonstrate the superiority of FL controllers in minimizing rise time, peak time, settling time, and steady-state error.

Keywords — DC Microgrid, Quadratic Boost Converter, PI Controller, FOPID, Fuzzy Logic Controller, Fault Analysis, THD, MATLAB/Simulink.

I. INTRODUCTION

Microgrids have emerged as a promising solution for decentralized energy systems, offering enhanced reliability, efficiency, and integration of renewable sources. They operate in grid-connected or standalone modes, supporting AC or DC distribution systems. DC microgrids are especially advantageous when interfacing with DC output sources like PV, fuel cells, and energy storage systems. However, challenges in fault detection and control stability remain significant.

This work proposes a DC microgrid architecture using a Quadratic Boost Converter (QBC) and evaluates system performance under various fault conditions. Furthermore, advanced control strategies including PI, FOPID, and FL controllers are employed to enhance output regulation and robustness against disturbances.

II. SYSTEM ARCHITECTURE AND METHODOLOGY

The proposed DC microgrid includes interconnected sources—PV, wind turbines, batteries, and fuel cells—coupled through a QBC. MATLAB/Simulink is used to simulate both healthy and faulty conditions, and controllers are applied in closed-loop configurations to regulate the output.

A. Fault Conditions

- Shorted Switch Fault: Reduced output voltage and power observed (20V, 8W) compared to the healthy system (67V, 90W).
- Line-to-Ground Fault: Induced 47.95% Total Harmonic Distortion (THD) in source current.
- Line-to-Line Fault: Reduced THD to 39.18%, indicating improved current quality.

B. Control Approaches

- PI Controller: Conventional method with notable steady-state error.
- FOPID Controller: Improves rise time (0.66s) and settling time (0.96s) over PI.
- Fuzzy Logic Controller: Best performance with rise time of 0.18s and steady-state error of 0.35V.

III. DC MICROGRID IN HEALTHY CONDITION AND SHORT-CIRCUITED SWITCH FAULT

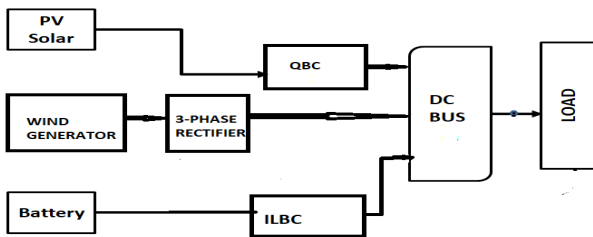


Fig.1. Modified block diagram

Simulation Results: DC Microgrid in healthy condition is presented in Fig.2. Voltage across PV is presented in Fig.3 and its value is 16V. Voltage across battery is presented in Fig.4 and its value is 15V. Voltage across R load is presented in Fig.5 and its value is 68V. Current through R load is presented in Fig.6 and its value is 1.4A. Output Power is presented in Fig.7 and its value is 90W.

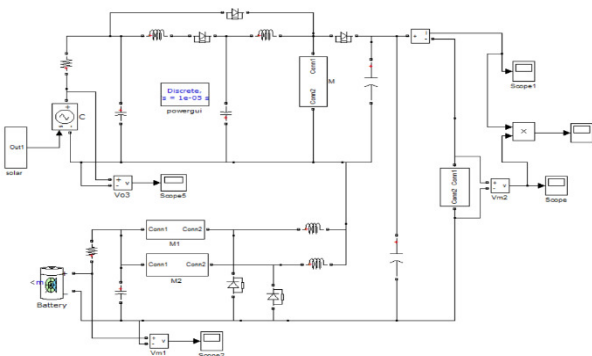


Fig.2 DC Microgrid in healthy condition

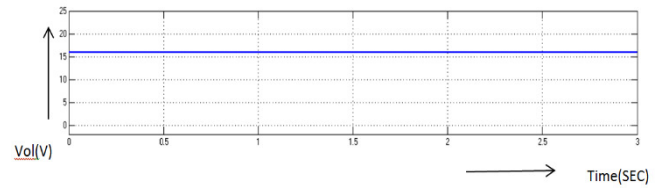


Fig.3 Voltage across PV

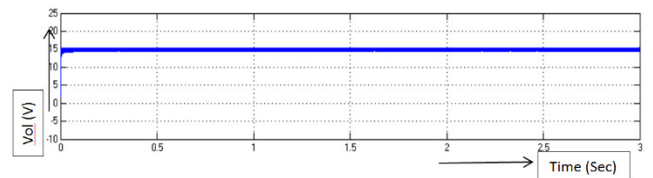


Fig.4 Voltage across battery

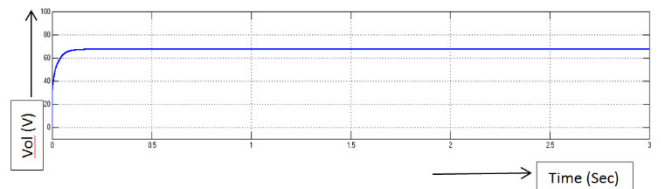


Fig.5 Voltage across R load

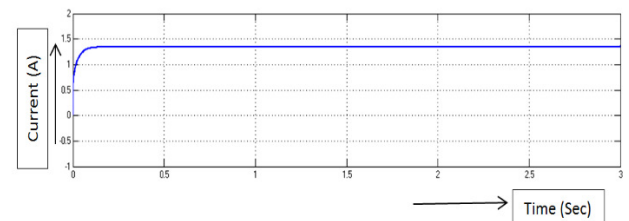


Fig.6 Current through R load

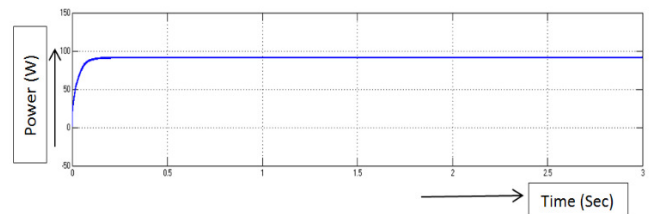


Fig.7 Output Power

IV. DC MICROGRID WITH LINE TO GROUND FAULT AND DC MICROGRID WITH LINE TO LINE FAULT

Simulation Results: DC Microgrid with line to ground fault is presented in Fig 8. Current of wind generator is presented I n Fig 9 & its value is 34A. Input current THD is presented in Fig 10 & its value is 47.95%.

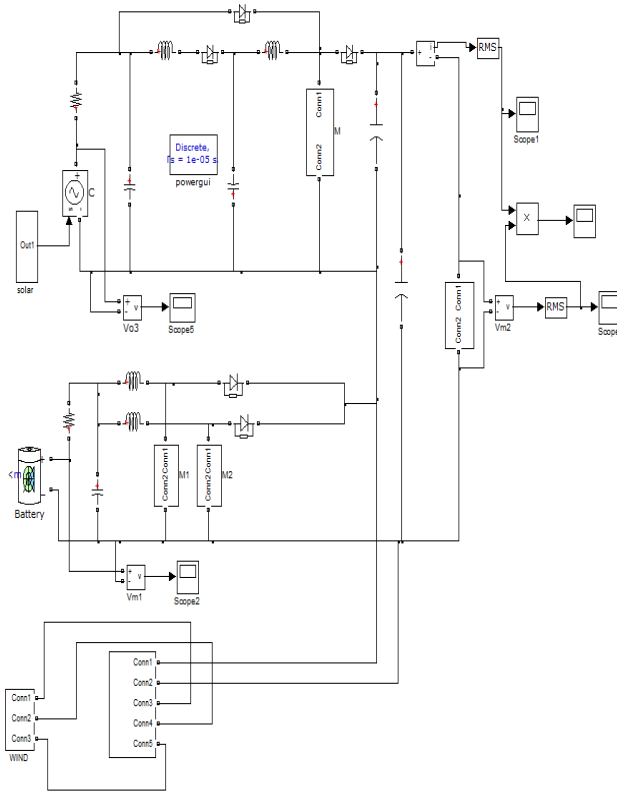


Fig.8 DC Microgrid with line to ground fault

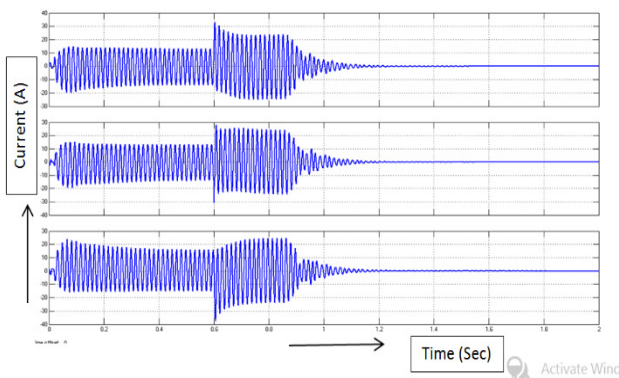


Fig.9 Current of wind generator

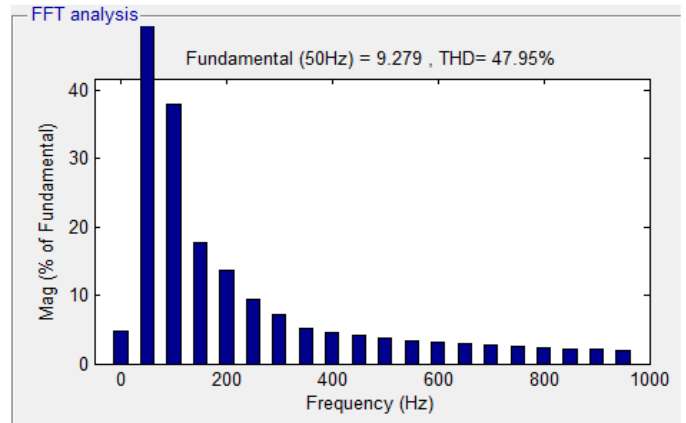


Fig.10 Input current THD

V. PI AND FOPID CLOSED LOOP DC MICRO-GRID

Simulation Result: Open loop DC micro-grid with source disturbance is delineated in fig.11. Input voltage with disturbance is delineated in fig. 12 and its value is 23V. Voltage across R-load with disturbance is delineated in fig.13 and its value is 118V. Current through R-load with disturbance is delineated in fig.14 and its value is 2.3A. Output power with disturbance is delineated in fig.15 and its value is 270W.

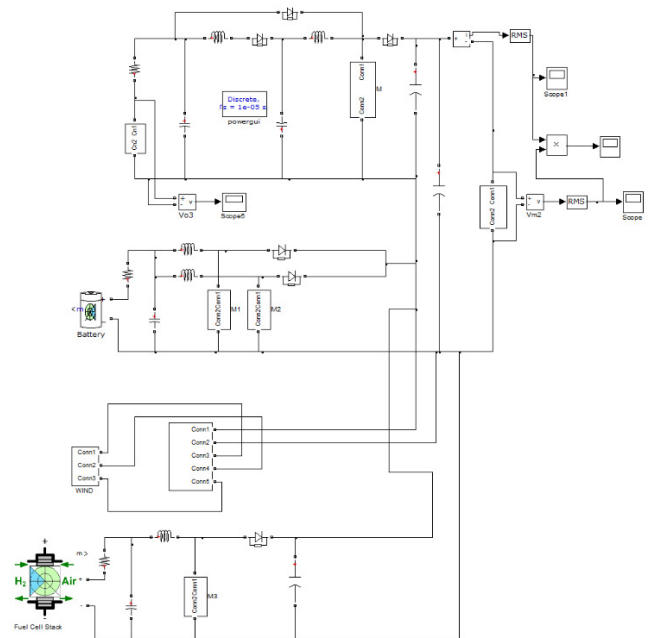


Fig.11 Open loop DC micro-grid with source disturbance

it can be seen that the output voltage, current and power are regulated and the closed loop system rejects the change in input voltage.

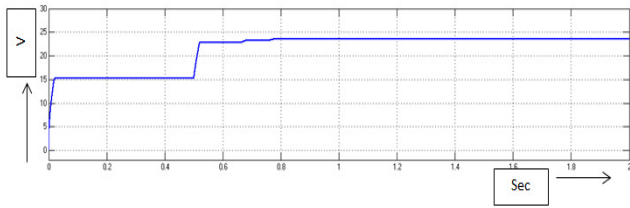


Fig.12 Input voltage with disturbance

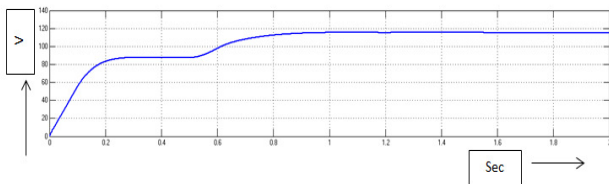


Fig.13 Voltage across R-load with disturbance

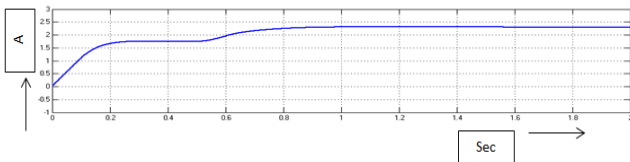


Fig.14 Current through R-load with disturbance

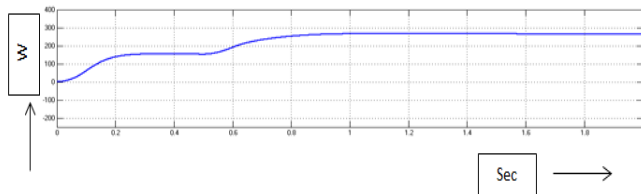


Fig.15 Output power with disturbance

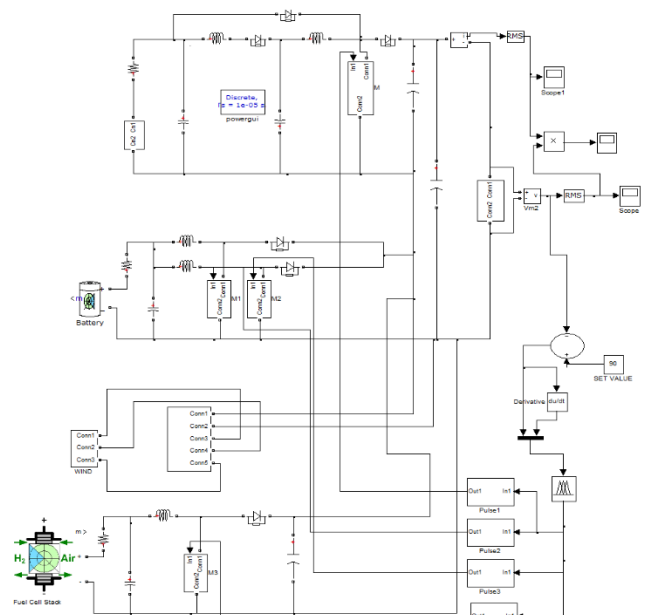


Fig.16 Closed loop DC micro-grid with Fuzzy Logic controller

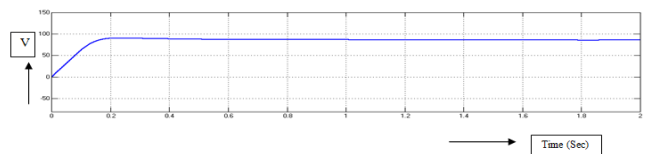


Fig.17 Voltage across R-load with Fuzzy Logic controller

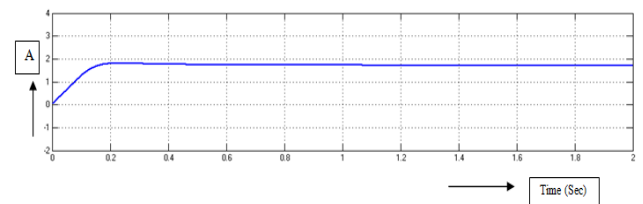


Fig.18 Current through R-load with Fuzzy Logic controller

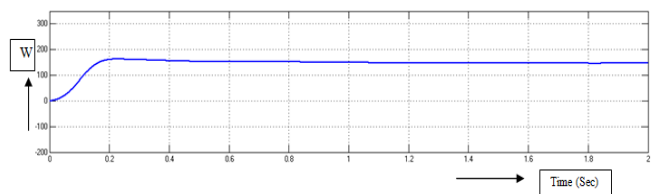


Fig.19 Output power with Fuzzy Logic controller

VI. FLC CONTROLLED CLOSED LOOP DC MICRO-GRID

Simulation Results: Closed loop DC micro-grid with FL controller is delineated in Fig. 16 Voltage across R-load with FL controller is delineated in Fig 17 and its value is 90V. Current through R-load with FL controller is delineated in Fig 18 and its value is 1.9A. Output power with FL controller is delineated in Fig 19 and its value is 160W. From the simulation results,

Comparison of Time Domain Parameters is delineated in Table 1. By using FL controller, rise time is reduced from 0.66 Sec to 0.18 Sec; peak time is reduced from 0.76 Sec to 0.22Sec; settling time is reduced from 0.96 Sec to 0.55 Sec; steady state error is reduced from 1.23V to 0.35V. Bar chart comparison of Time Domain Parameters is delineated in Fig. 20.

TABLE I
 Comparison of Time Domain Parameters

Controller	Tr	Ts	Tp	Ess
FOPID	0.66	0.96	0.76	1.23
FLC	0.18	0.55	0.22	0.35
Controller	Tr	Ts	Tp	Ess

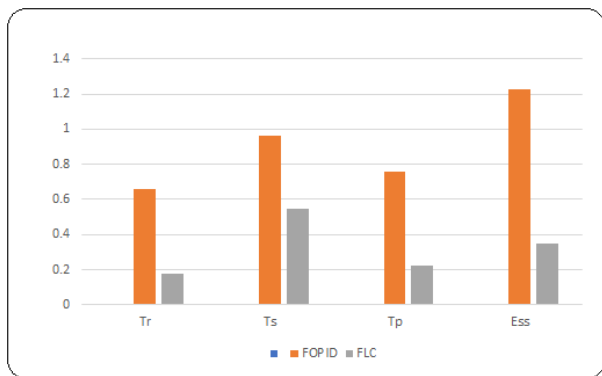


Fig.20 Bar chart comparison of Time Domain Parameters

VII. CONCLUSION

This work mainly deals with the design, plan and comparison of DC micro grid in healthy condition and DC microgrid in short circuited switch fault. The outcomes are compared in terms of output voltage, output current and output power. In faulty condition, output voltage, output current and output power are reduced.

This work also presents the design, plan and comparison of DC microgrid with line to ground fault and DC microgrid with line to line fault . The outcomes are compared in terms of Current THD. With Line to line fault, current THD is 47.95% and

with Line to ground fault, current THD is 39.18%. Hence, the outcomes represents that the DC Microgrid with line to line fault produces higher THD when compared to DC Microgrid with line to ground fault.

Simulation results with shorted fault in boost converter indicate fall in grid voltage and output power. Open loop and closed loop QBC with PV, wind, battery and Fuel cell with PI/ FOPID controller are analyzed and simulated. By using FOPID controller, rise time is reduced from 0.75 Sec to 0.66Sec; peak time is reduced from 0.83 Sec to 0.76Sec; settling time is reduced from 1.20 Sec to 0.96 Sec; steady state error is reduced from 1.78V to 1.23V. Hence, the outcome represents that closed loop DC micro-grid with FOPID controller is superior to closed loop DC micro-grid with PI controller.

Closed loop DC microgrid with FOPID/FLC controller are analyzed and simulated. By using-FLC controller, rise time is reduced from 0.66Sec to 0.18 Sec; peak time is reduced from 0.76 Sec to 0.22 Sec; settling time is reduced from 0.96 Sec to 0.55 Sec; steady state error is reduced from 1.23V to 0.35V. Hence, the outcome represents that closed loop DCMGS with FL controller is superior to closed loop DCMGS with FOPID.

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